

Thermodynamics I

Chapter 4

First Law of Thermodynamics

Open Systems

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First Law of Thermodynamics (Motivation)

A system changes due to interaction with its surroundings.

Interaction study is possible due to conservation laws.

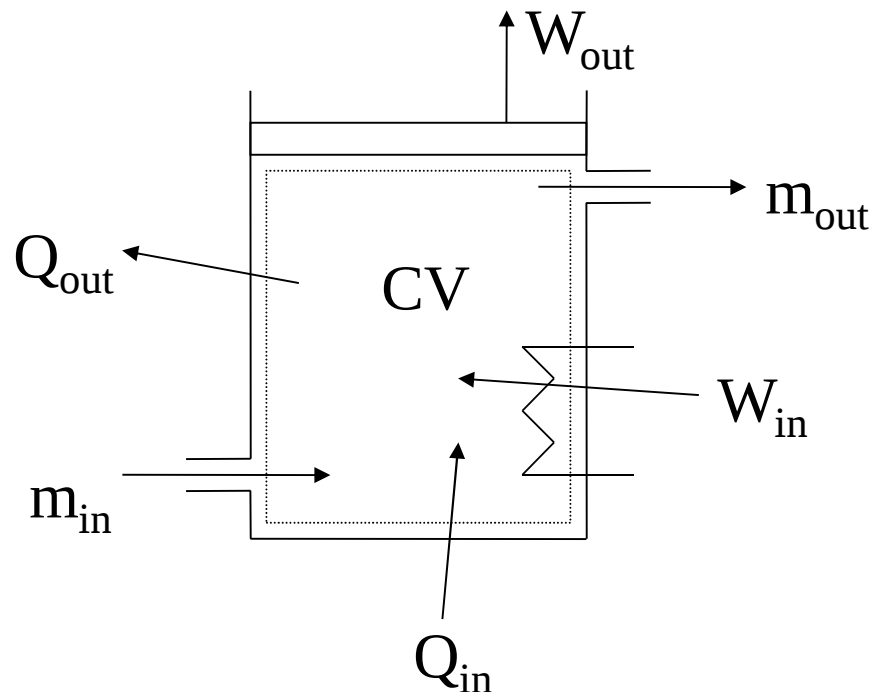
Various forms of conservation laws are studied in this chapter in the form of balance equations.

1ST LAW FOR OPEN SYSTEMS

Energy and Mass can enter/leave a system

Divided into two parts:

- Conservation of Mass Principle
- Conservation of Energy Principle



Mass Conservation (Mass Balance)

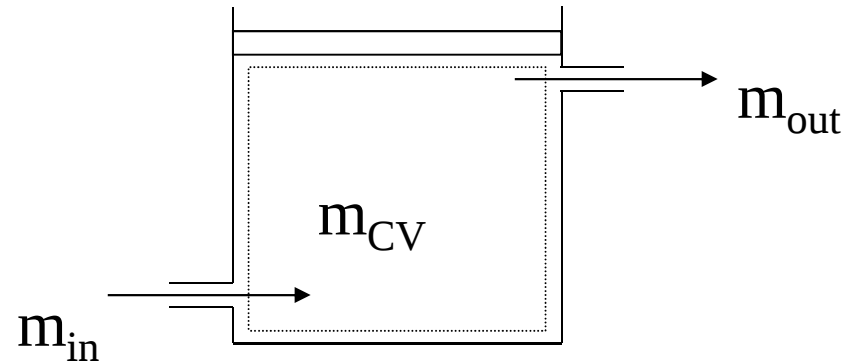
Mass Balance:

$$\Delta m_{CV} = \sum m_{in} - \sum m_{out}$$

Net change
of mass of
CV

Total of all
mass entering

Total of all
mass exiting



$$\frac{dm_{CV}}{dt} = \sum \frac{dm_{in}}{dt} - \sum \frac{dm_{out}}{dt}$$

Rate of
change of
mass of
CV

Total of all mass
flow rates for all
inlet channels

Total of all mass
flow rates for all
exit channels

Mass flow rates and Speed for a channel

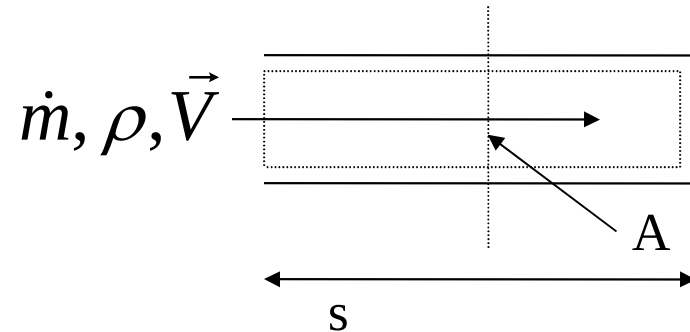
$$m = \rho V$$

$$m = \rho s A$$

For flow rates;

$$\frac{dm}{dt} = \rho \frac{ds}{dt} A$$

$$\dot{m} = \rho \vec{V} A$$



but

$$sA = V$$

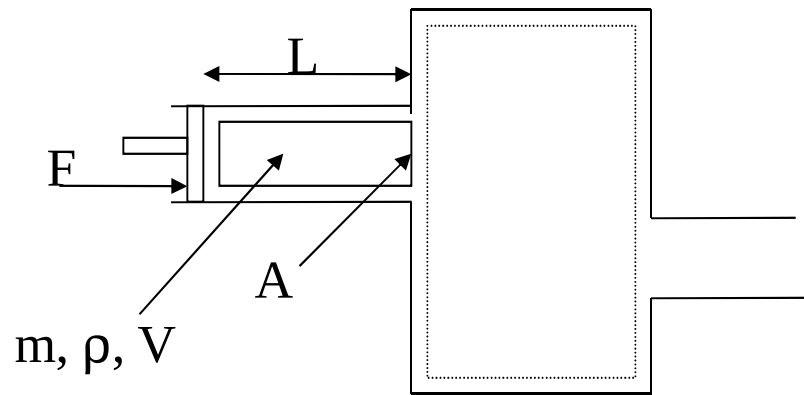
Thus;

$$\dot{m} = \rho \vec{V} A = \frac{\vec{V} A}{v} = \rho \dot{V} = \frac{\dot{V}}{v}$$

$$\frac{ds}{dt} A = \dot{V}$$

Flow Work

For an amount of mass to cross a boundary, it needs a force (work) to push it; called Flow Work , w_{flow}



The force that pushes the fluid;

$$F = PA$$

Work that is involved;

$$W = \int F \cdot ds$$

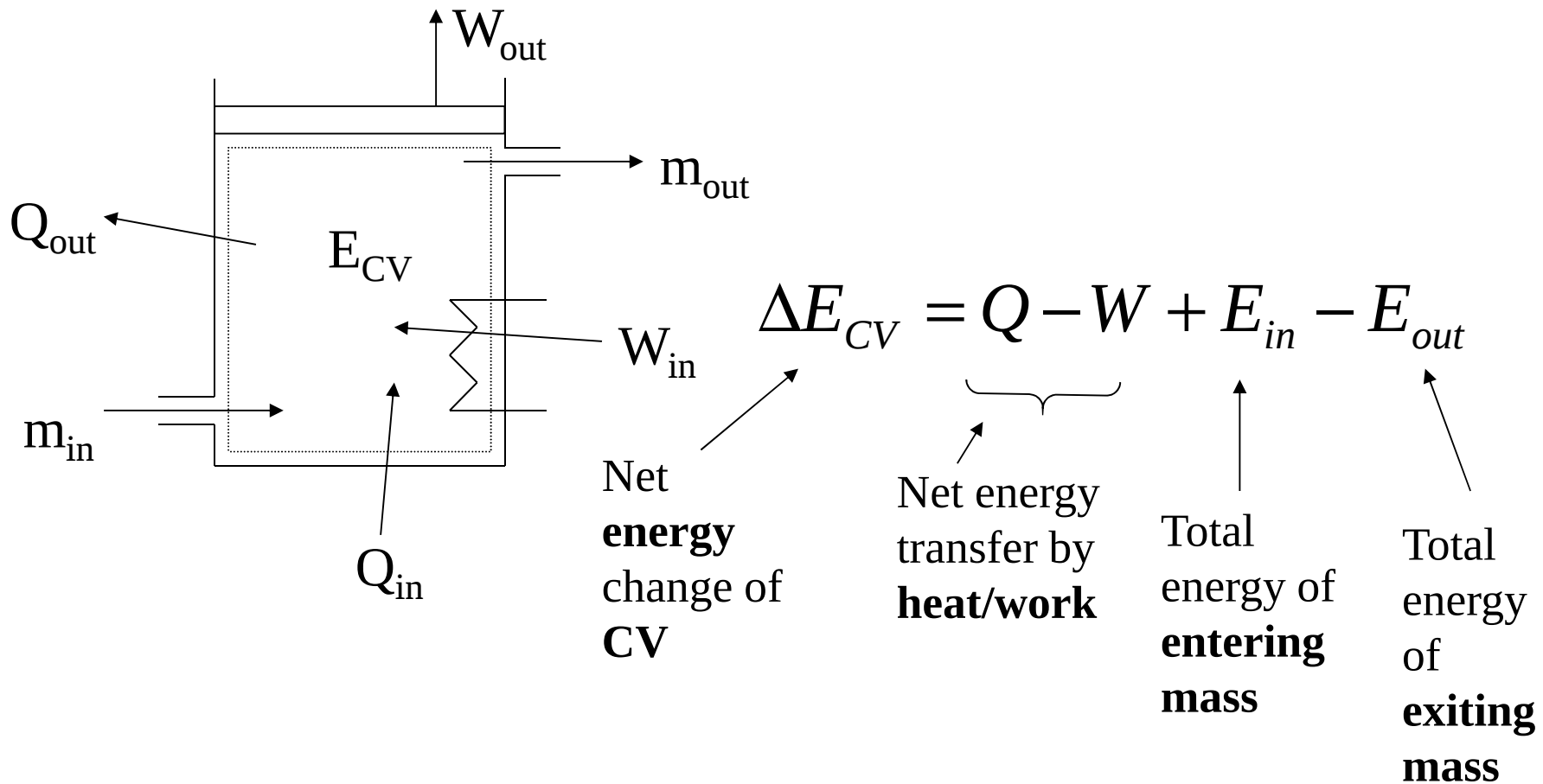
$$\begin{aligned} W_{\text{flow}} &= F \cdot L \\ &= PA \cdot L \\ &= PV \end{aligned}$$

$$w_{\text{flow}} = pv$$

Conservation of Energy for Open Systems

Energy can enter/leave an open system via

Heat, Work AND Mass Flow Entering/Leaving



Energy of a Flowing Mass

An amount of mass possesses energy, E , e

$$e = u + ke + pe$$

but a flowing mass also possesses flow work, so

the Energy for a flowing mass; e_{flow}

$$\begin{aligned} e_{\text{flow}} &= u + ke + pe + w_{\text{flow}} \\ &= u + pv + ke + pe \end{aligned}$$

but $u + pv = h$ (enthalpy)

$e_{\text{flow}} = \mathbf{h + ke + pe}$

 (energy for a flowing mass)

Energy Balance for an Open System

can be written as;

$$\Delta E_{CV} = Q - W + E_{flow_{in}} - E_{flow_{out}}$$

or;

$$\begin{aligned}\Delta e_{CV} &= q - w + e_{flow_{in}} - e_{flow_{out}} \\ &= q - w + (h + ke + pe)_{in} - (h + ke + pe)_{out} \\ &= q - w + \sum_{in} (h + ke + pe) - \sum_{out} (h + ke + pe)\end{aligned}$$

Total of all work
except flow work

For each
inlet

For each
outlet

but;

$$\Delta e_{CV} = (\Delta u + \Delta ke + \Delta pe)_{CV}$$

so;

$$\begin{aligned} (\Delta u + \Delta ke + \Delta pe)_{CV} &= q - w \\ &+ \sum_{in} (h + ke + pe) - \sum_{out} (h + ke + pe) \end{aligned}$$

Energy Balance in other forms;

$$\Delta E_{CV} = Q - W + \sum_{in} (H + KE + PE) - \sum_{out} (H + KE + PE)$$

Rate form;

$$\frac{dE_{CV}}{dt} = \dot{Q} - \dot{W} + \sum_{in} \dot{m}(h + ke + pe) - \sum_{out} \dot{m}(h + ke + pe)$$

↑
(general form of Energy Balance for an
Open System)

Steady Flow Process

Criteria;

All system properties (intensive & extensive)

do not change with time

$$m_{cv} = \text{constant}; \Delta m_{cv} = 0$$

$$V_{cv} = \text{constant}; \Delta V_{cv} = 0$$

$$E_{cv} = \text{constant}; \Delta E_{cv} = 0$$

Fluid properties at all inlet/exit channels do not change with time (Values might be different for different channels)

$$(\dot{m}, \vec{V}, A, \text{etc.})$$

Heat and work interactions do not change with time

$$\dot{Q} = \text{constant}$$

$$\dot{W} = \text{constant}$$

Implication of Criterion 1

(**Mass**)

$$\Delta m_{CV} = 0,$$

From Mass Conservation;

$$\sum \dot{m}_{in} - \sum \dot{m}_{out} = \Delta m_{CV}$$

$$\therefore \boxed{\sum \dot{m}_{in} = \sum \dot{m}_{out}}$$

Recall that

$$\dot{m} = \rho \vec{V} A = \frac{\vec{V} A}{v}$$

so

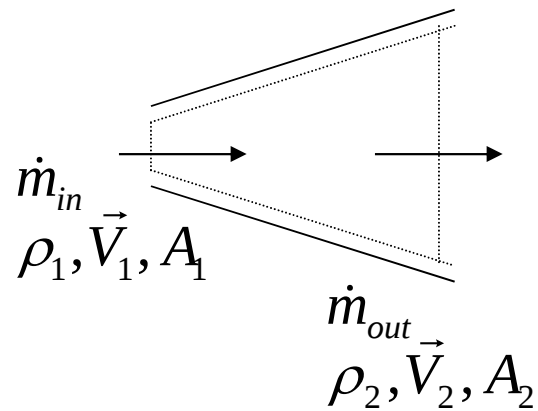
$$\boxed{\sum_{i=1}^n \rho_i \vec{V}_i A_i \Big|_{in} = \sum_{o=1}^k \rho_o \vec{V}_o A_o \Big|_{out}}$$

$$\dot{m}_{in} = \dot{m}_{out}$$

$$\rho_1 \vec{V}_1 A_1 = \rho_2 \vec{V}_2 A_2$$

Implication of Criterion 1 (**Mass**) ctd.

for 1 inlet/ 1 exit;



Implication of Criterion 1

(Volume)

$$\Delta V_{CV} = 0,$$

$$\therefore W_B = 0 (\text{boundary work} = 0)$$

$$\Delta E_{CV} = Q - W + \Sigma E_{\text{flow(in)}} - \Sigma E_{\text{flow(out)}}$$

$$W = W_{\text{electrical}} + W_{\text{shaft}} + \cancel{W_{\text{boundary}}} + \cancel{W_{\text{flow}}} + W_{\text{etc.}}$$

0
in h

W not necessarily 0, only W_B is 0

Implication of Criterion 1

(Energy)

$$\Delta E_{CV} = 0,$$

From Energy Conservation;

$$\frac{dE_{CV}}{dt} = \dot{Q} - \dot{W} + \sum_{in} \dot{m}(h + ke + pe) - \sum_{out} \dot{m}(h + ke + pe)$$

↙
→ = 0

Rearrange to get Steady Flow Energy Equation

(SSSF)

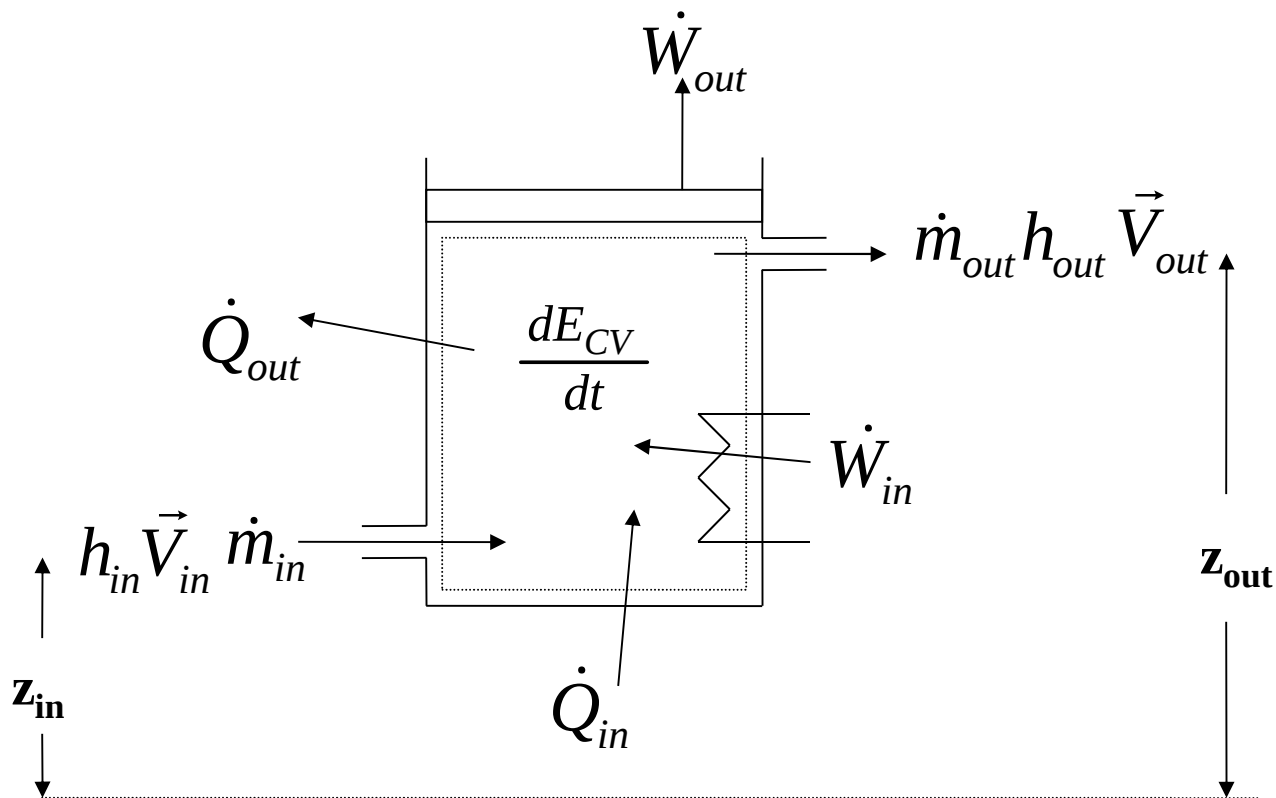
$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

SSSF

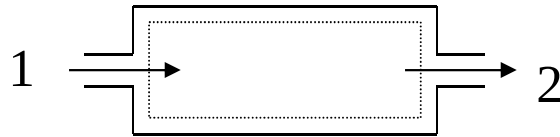
$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left(h + \frac{\vec{V}^2}{2} + gz \right) - \sum_{in} \dot{m} \left(h + \frac{\vec{V}^2}{2} + gz \right)$$

For each **exit**
channel

For each **inlet**
channel



SSSF energy equation for 1 inlet / 1 exit



Mass

$$\dot{m}_{in} = \dot{m}_{out} \quad \text{or} \quad \dot{m}_1 = \dot{m}_2$$

Energy

$$\dot{Q} - \dot{W} = \dot{m}_2 \left(h_2 + \frac{\vec{V}_2^2}{2} + gz_2 \right) - \dot{m}_1 \left(h_1 + \frac{\vec{V}_1^2}{2} + gz_1 \right)$$

$$\dot{m}_1 = \dot{m}_2 = \dot{m}$$

$$\dot{Q} - \dot{W} = \dot{m} \left[(h_2 - h_1) + \left(\frac{\vec{V}_2^2 - \vec{V}_1^2}{2} \right) + g(z_2 - z_1) \right]$$

$$\frac{\dot{Q}}{\dot{m}} - \frac{\dot{W}}{\dot{m}} = (h_2 - h_1) + \left(\frac{\vec{V}_2^2 - \vec{V}_1^2}{2} \right) + g(z_2 - z_1)$$

$$q - w = \Delta h + \Delta ke + \Delta pe \quad (1 \text{ inlet} / 1 \text{ exit}) \quad (\Delta = \text{exit} - \text{inlet})$$

SSSF energy equation for multiple channels but neglecting Δke , Δpe

$$\dot{Q} - \dot{W} = \sum \dot{m}_{out} h_{out} - \sum \dot{m}_{in} h_{in}$$

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

SSSF Applications

For devices which are *open systems*

- (a) { Nozzle & Diffuser
Turbine & compressor
Throttling valve @ porous plug
- (b) { Mixing/Separation Chamber
Heat exchanger(boiler, condenser, etc)

2 categories;

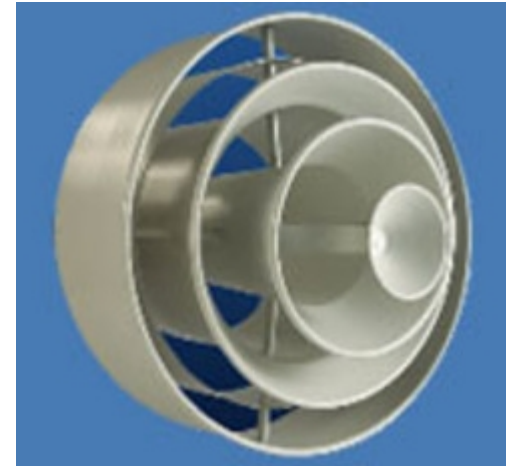
1 inlet / 1 outlet

Multiple inlet / outlet

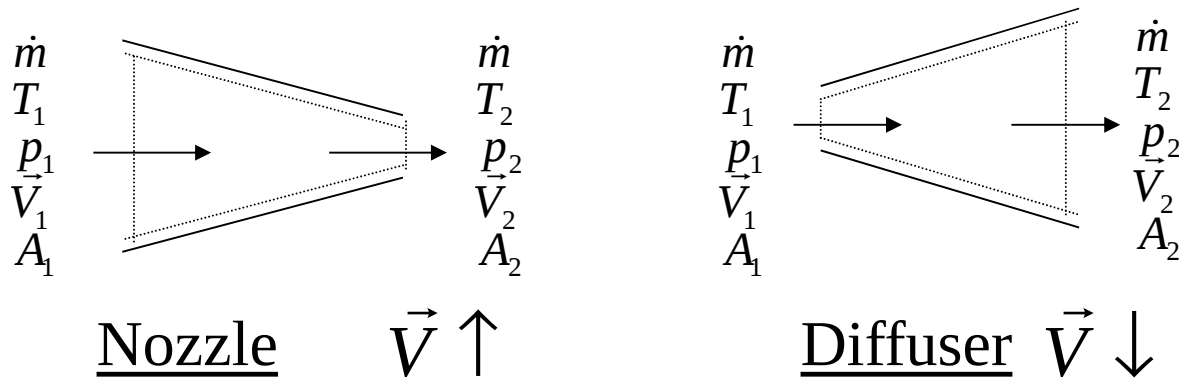
Analysis starts from the general SSSF energy equation;

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

Nozzle & Diffuser ($\Delta KE \neq 0$) (To change fluid velocity)



Nozzle & Diffuser ($\Delta KE \neq 0$) (To change fluid velocity)



Assumptions

Const. volume $\rightarrow w_B = 0$
 No other work

$$\left. \begin{array}{l} \text{Const. volume } \rightarrow w_B = 0 \\ \text{No other work} \end{array} \right\} w_{CV} = 0$$

Small difference in height $\rightarrow \Delta pe = 0$

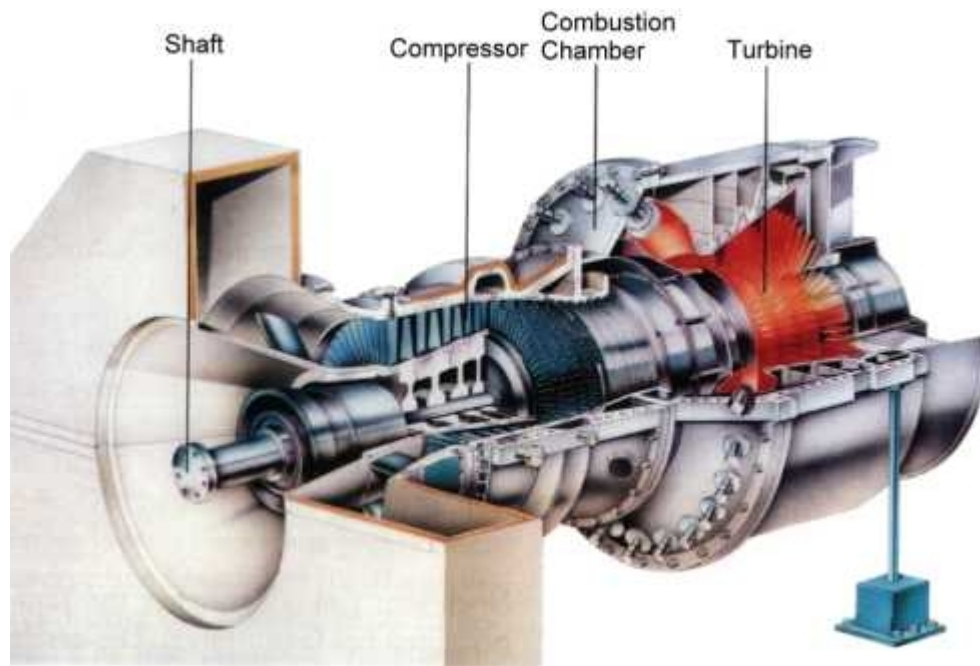
$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

1 inlet / 1 outlet

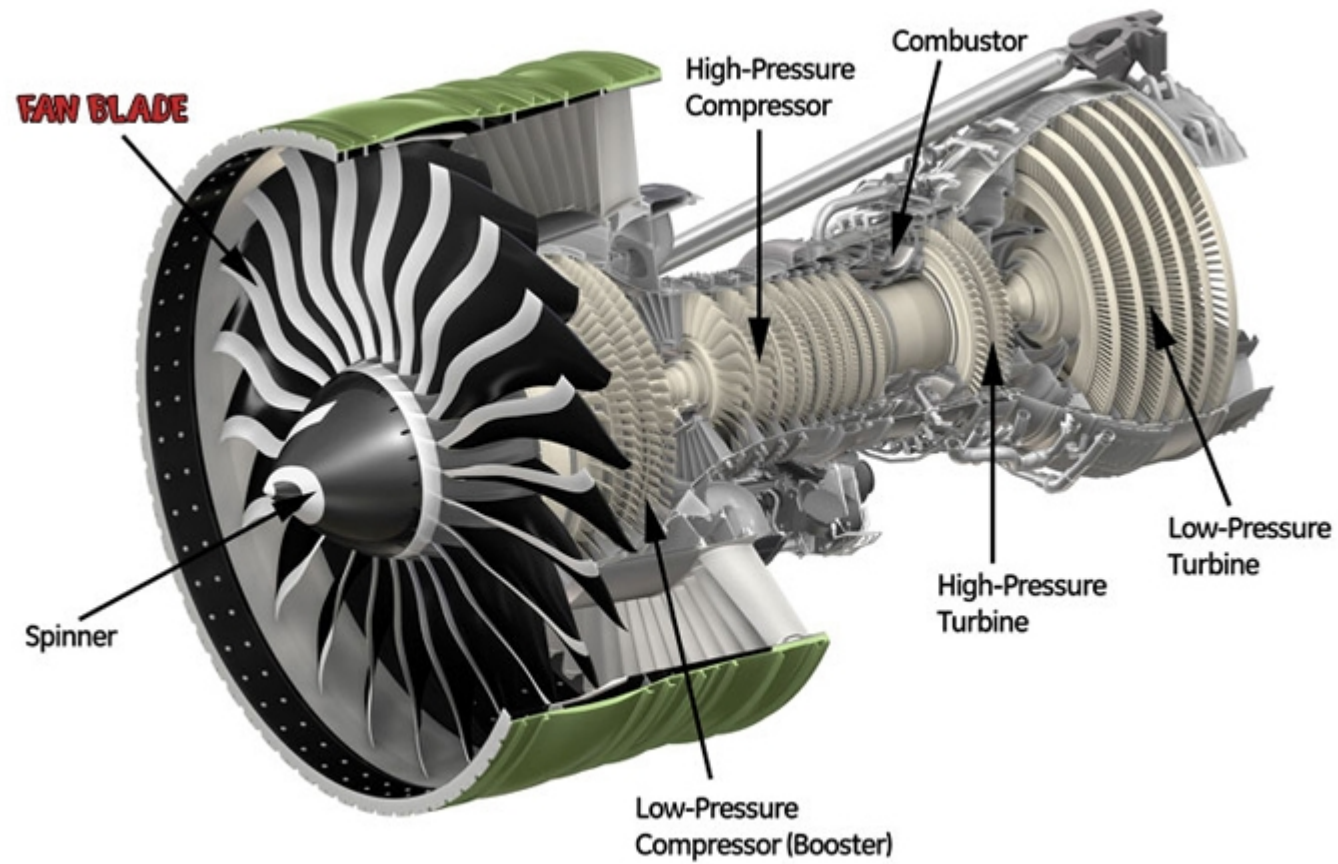
$$q - \cancel{w} = \Delta h + \Delta ke + \cancel{\Delta pe}$$

$$q = \Delta h + \Delta ke$$

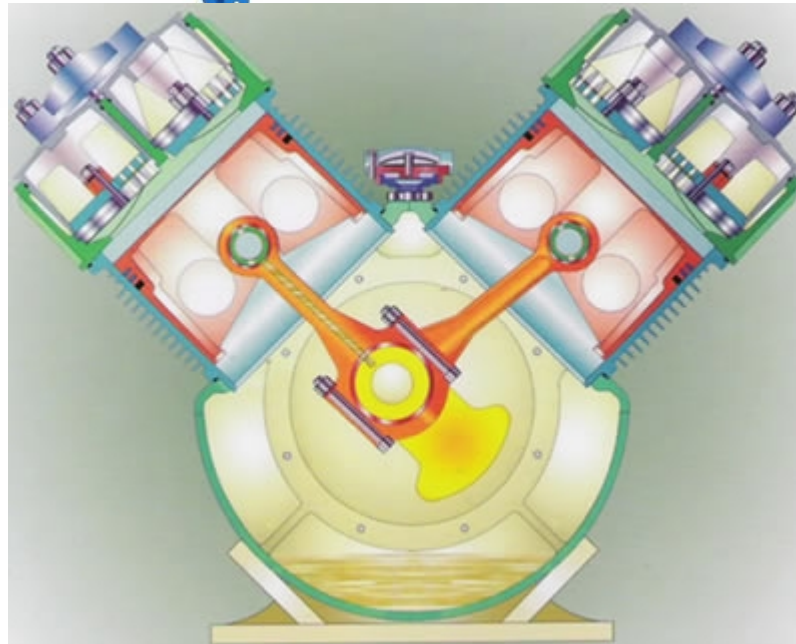
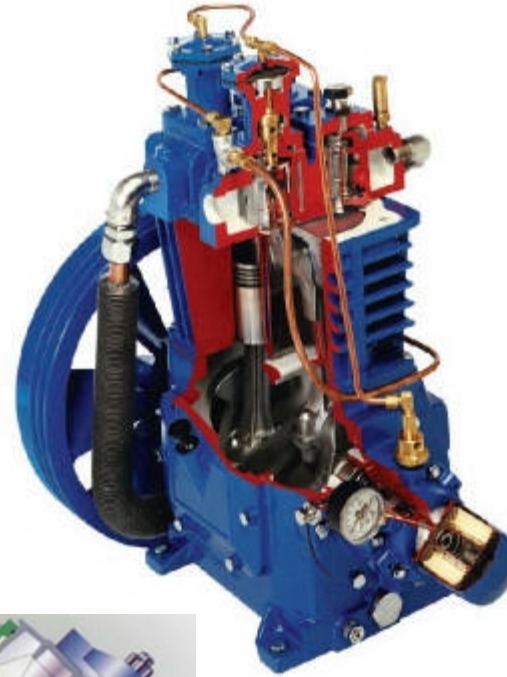
Turbine ($w_{CV} \neq 0$)



Turbine & Compressors ($w_{CV} \neq 0$)

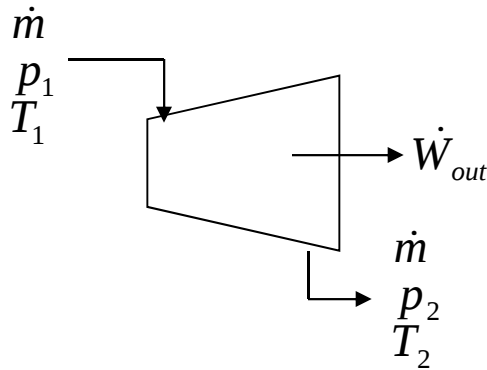


Compressors (Reciprocating) ($w_{CV} \neq 0$)



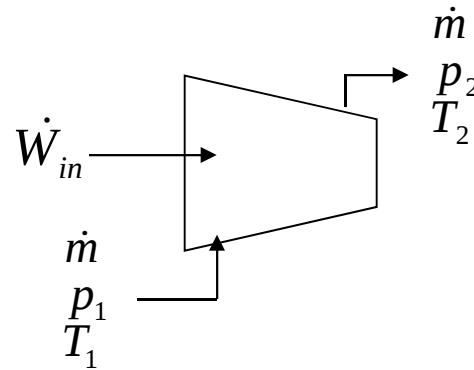
Turbine & Compressor

($w_{CV} \neq 0$)



Turbine

produces work (W +ve)
 from expansion of
 fluid (ΔP -ve)



Compressor

increases pressure (ΔP
 +ve) using work supplied
 (W -ve)

Assumptions

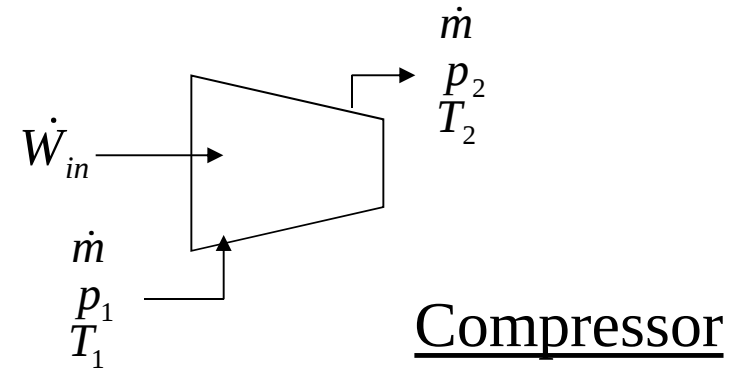
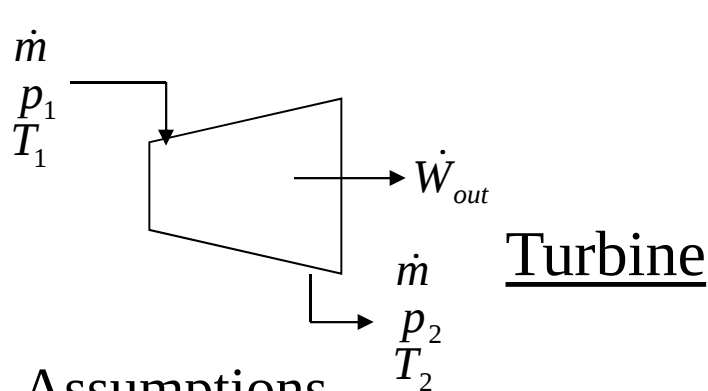
Const. volume $\rightarrow w_B = 0$

Involves other work

Small difference in height $\rightarrow \Delta p_e = 0$

} $w_{CV} \neq 0$

Turbine & Compressor ($w_{CV} \neq 0$)



Assumptions

Const. volume $\rightarrow w_B = 0$
 Involves other work
 Small difference in height $\rightarrow \Delta pe = 0$

} $w_{CV} \neq 0$

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

1 inlet / 1 outlet

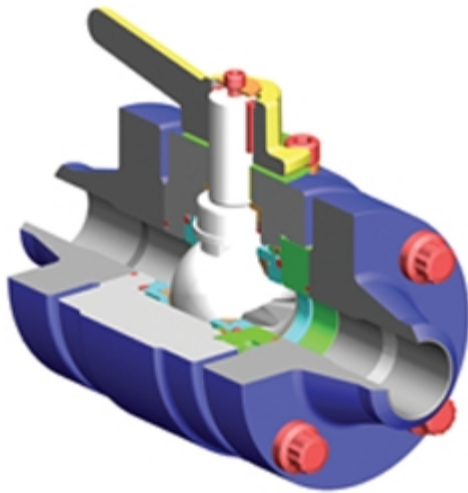
$$\dot{Q} - \dot{W} = \dot{m}(\Delta h + \Delta ke + \cancel{\Delta pe})$$

Commonly insulated ($q=0$), and also
 $\Delta ke \approx 0$ (since $\Delta ke \ll \Delta h$)

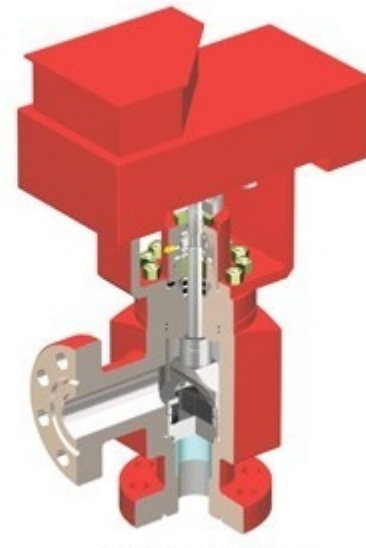
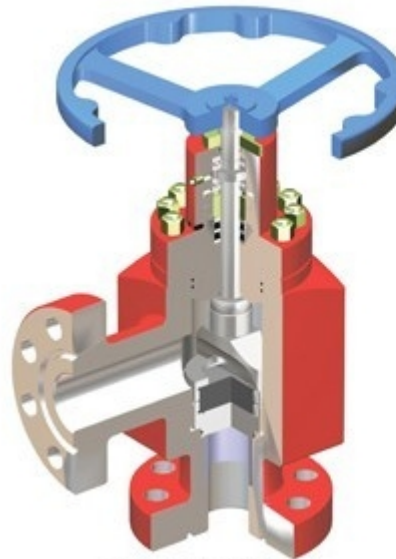
$$-\frac{\dot{W}}{\dot{m}} = \Delta h = h_2 - h_1$$

Throttling valve/Porous plug (const. enthalpy, $h=c$)

To reduce pressure without involving work

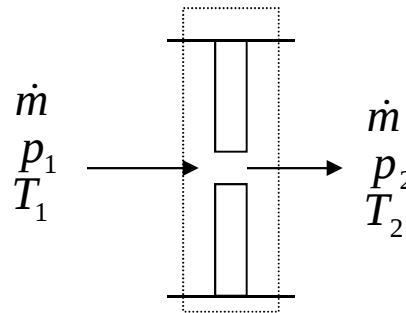
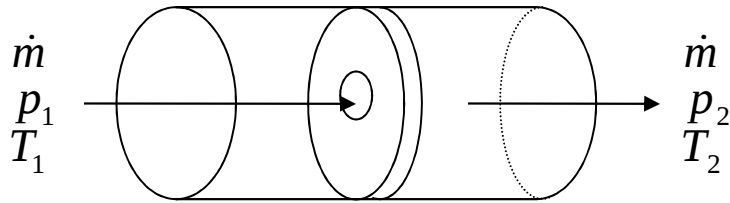


E-STORE 



Throttling valve/Porous plug (const. enthalpy, $h=c$)

To reduce pressure without involving work



Assumptions

$$W = 0$$

$$\Delta ke = 0, \Delta pe = 0$$

$Q \approx 0$ (system too small)

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

1 inlet / 1 outlet

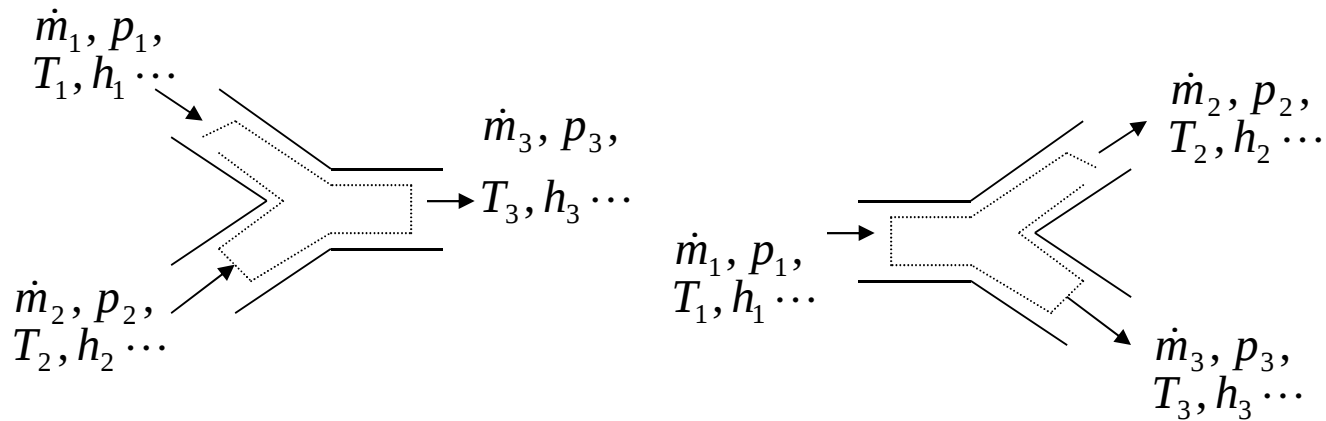
$$\cancel{\dot{q}} - \cancel{\dot{w}} = \Delta h + \cancel{\Delta ke} + \cancel{\Delta pe}$$

$$\Delta h = 0$$

$$h_1 = h_2$$

For throttling valves

Mixing/Separation Chamber / T junction pipe



Assumptions

$$W_B = 0$$

Same pressure at all channels

Other assumptions made accordingly

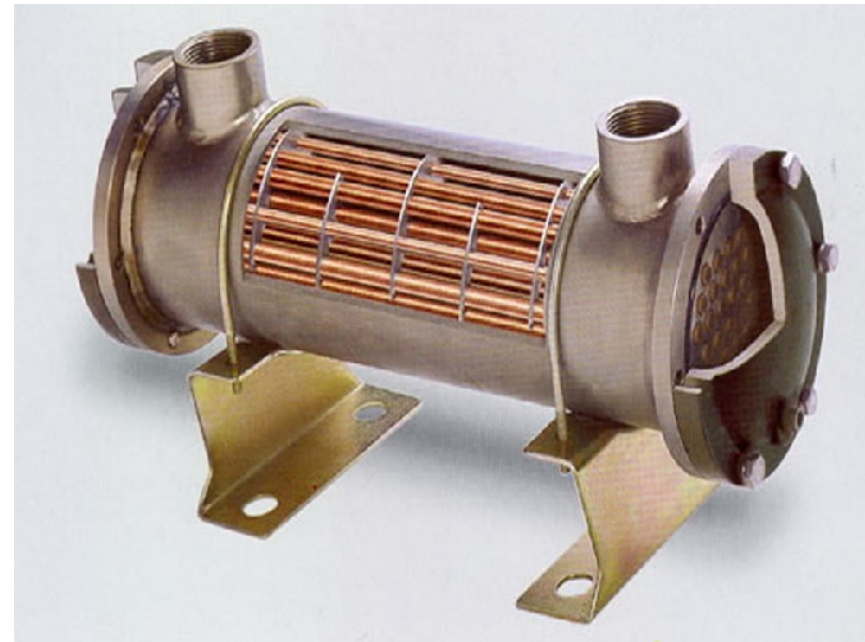
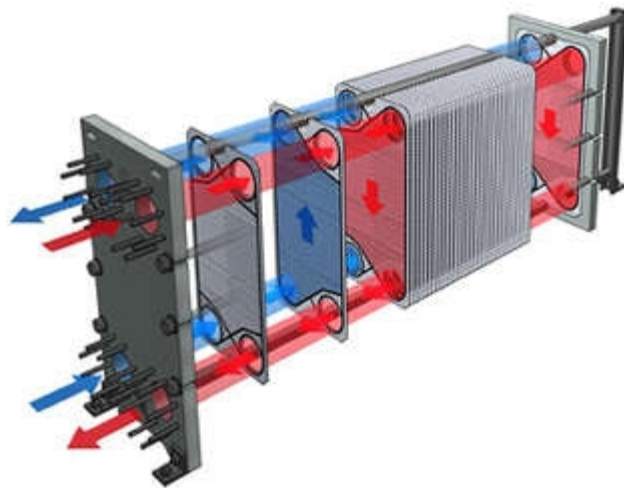
$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

also

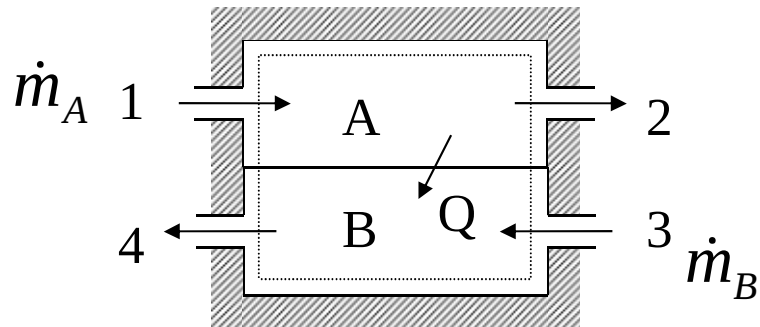
$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$



Heat Exchangers



Heat Exchangers



Assumptions (*System encompasses the whole heat exchanger*)

No work involved, $W = 0$

Insulated, $Q = 0$

$\Delta ke = 0$, $\Delta pe = 0$

$$\cancel{\dot{Q}} - \cancel{\dot{W}} = \sum_{out} \dot{m}(h + \cancel{ke} + \cancel{pe}) - \sum_{in} \dot{m}(h + \cancel{ke} + \cancel{pe})$$

$$\sum \dot{m}_{in} h_{in} = \sum \dot{m}_{out} h_{out}$$

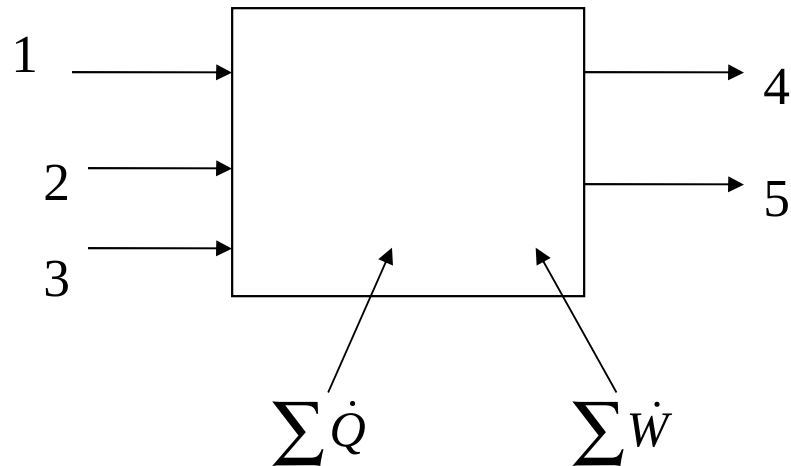
$$\dot{m}_A h_1 + \dot{m}_B h_3 = \dot{m}_A h_2 + \dot{m}_B h_4$$

$$\dot{m}_A (h_1 - h_2) = \dot{m}_B (h_4 - h_3)$$

also

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

General device (Black box analysis)



Assumptions made according to situation...

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

also

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$